



# IMPACT

EPSRC Centre for Doctoral Training in  
Innovative Metal Processing (IMPACT)

## The Effects of Deep Cryogenic Treatment on PVD – TiN coated AISI M2 high speed steel

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- *Background*
- *Motivation*
- *PhD Approach*
- *Experimental workflow*
- *Results*
- *Next step*
- *Conclusion*
- *References and Acknowledgement*



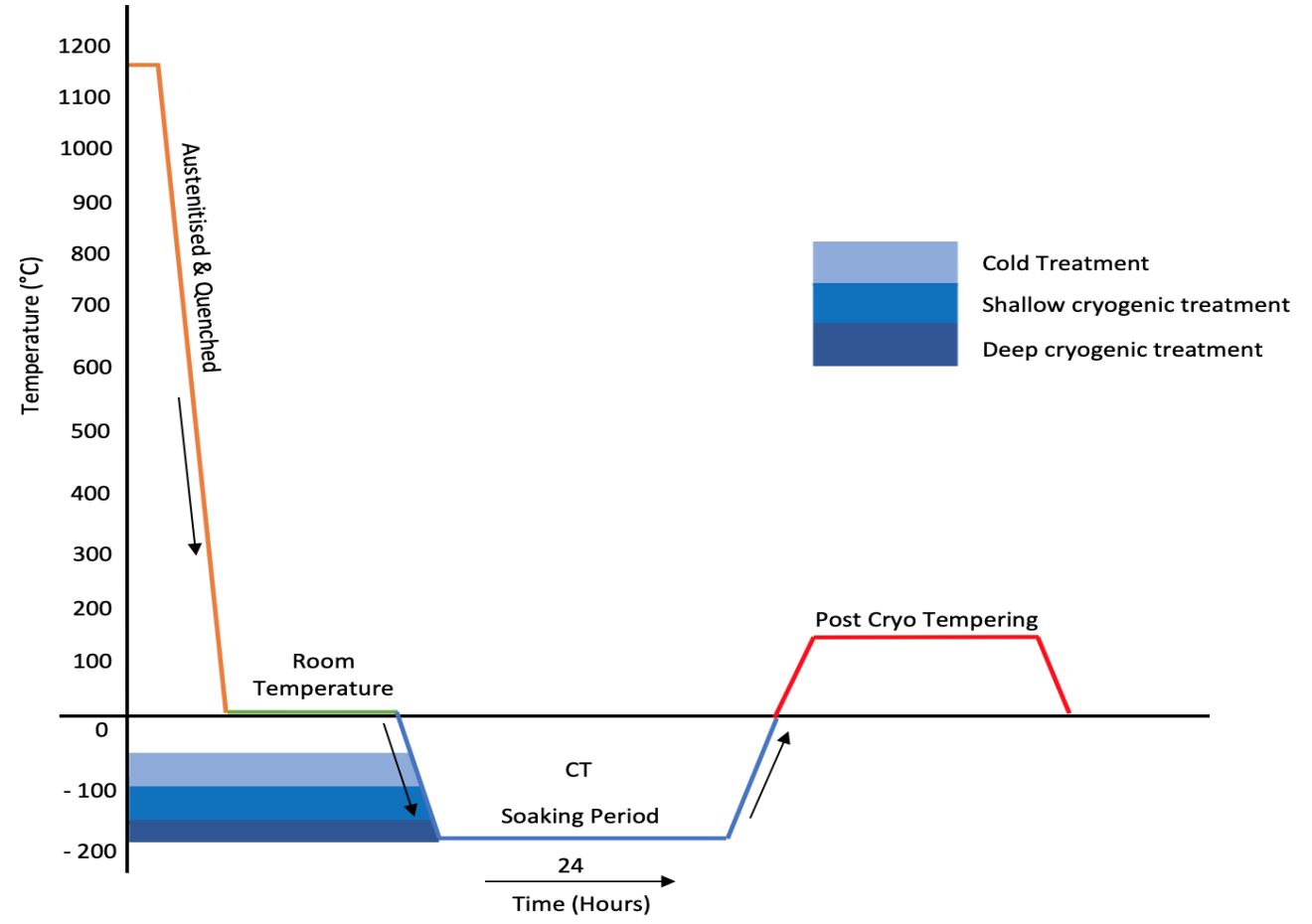
# Background



- *How we understand it*
- *213K to 193K (-60 to -80° C)*
- *193 to 113 K (-80 to -160° C)*
- *113 to 77 K (-160 to -196° C)*
- *CT practice*

*Industry: Restricted parameters, one cycle, varying practice – LN<sub>2</sub> or N<sub>2</sub>, large batches*

*Research: Entire process, small quantities, N<sub>2</sub> cooling medium*





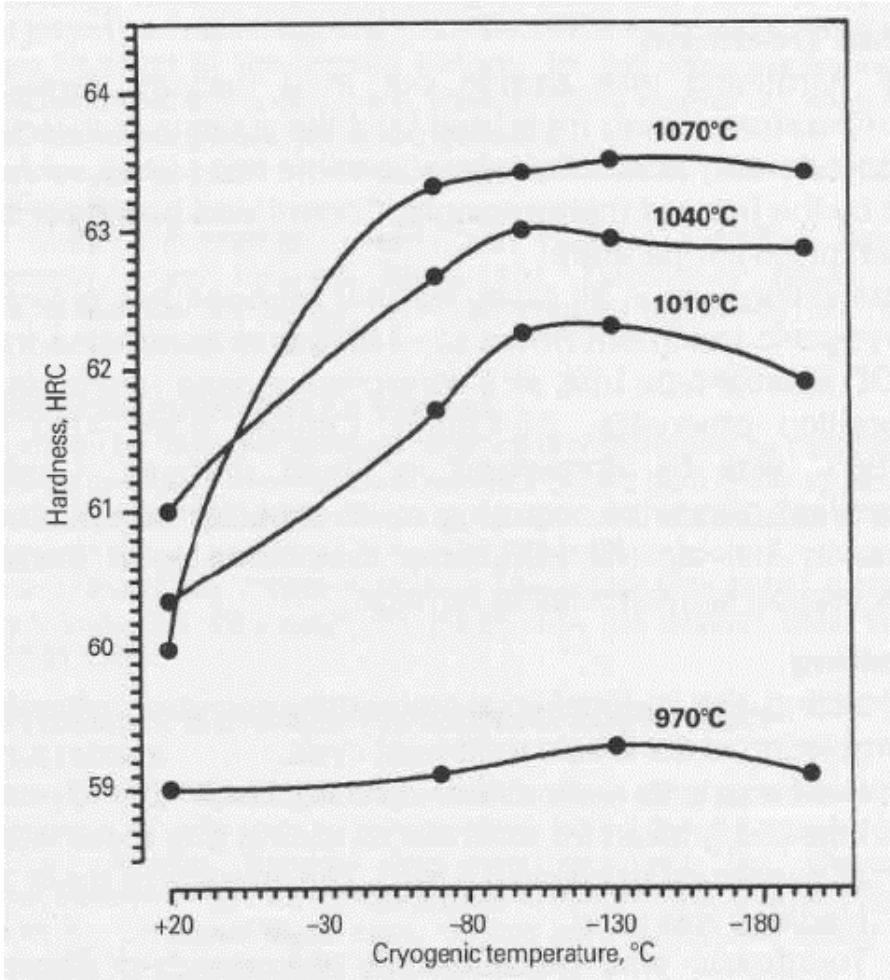
## ***CT Applications (Not limited to)***

- *Manufacturing – Cutting tools*
- *Automobile - Brake Discs, Gears*
- *Medical - knives*

*Some applications CT materials – coated*



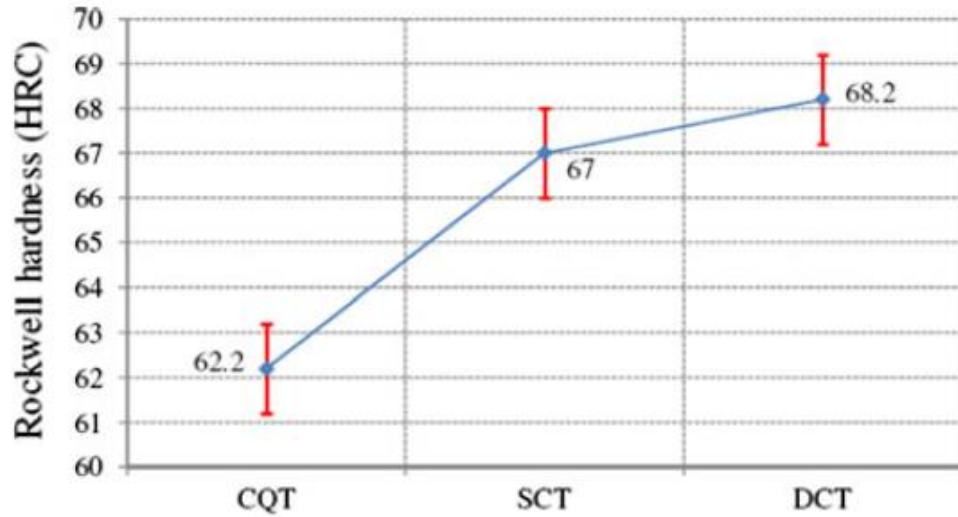
# Motivation



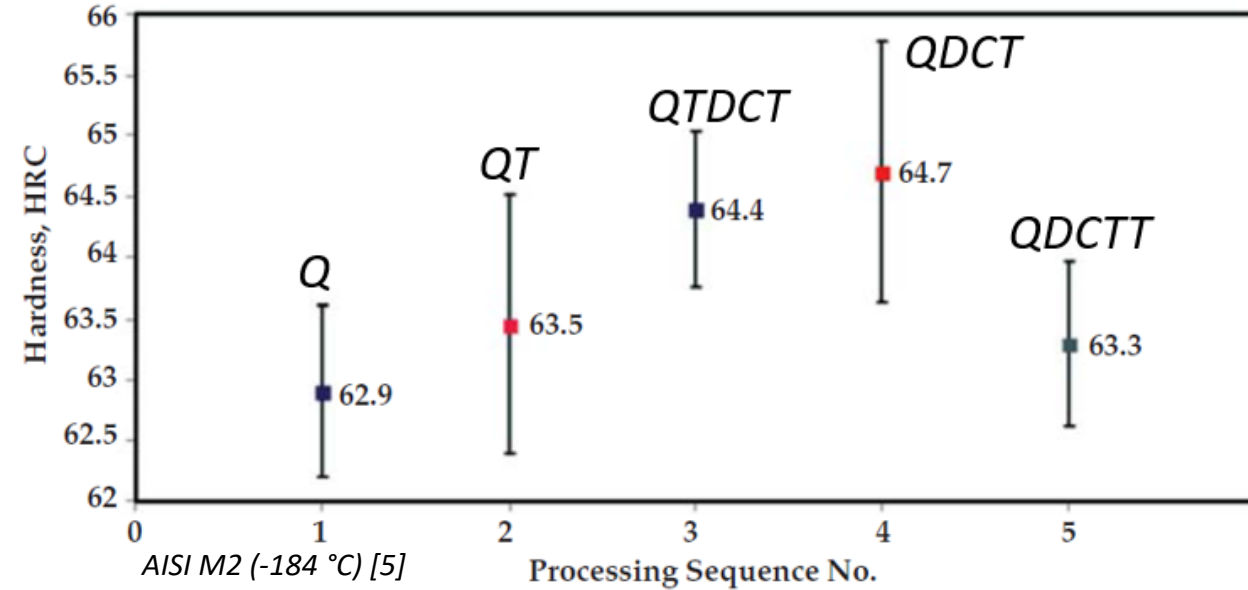
AISI D2	-80	63.4 HRC	Reference [1]
AISI D2	-196°C	63.7 HRC	Reference [2]

*AISI D2: Max Hardness (-80 to -110 °C) [1]*

# Motivation



AISI M2: (-196 °C) [3] Type of heat treatment



AISI M2 (-184 °C) [5]

Effect of the cryogenic treatment on the tool hardness AISI M2: (-196 °C) [4]

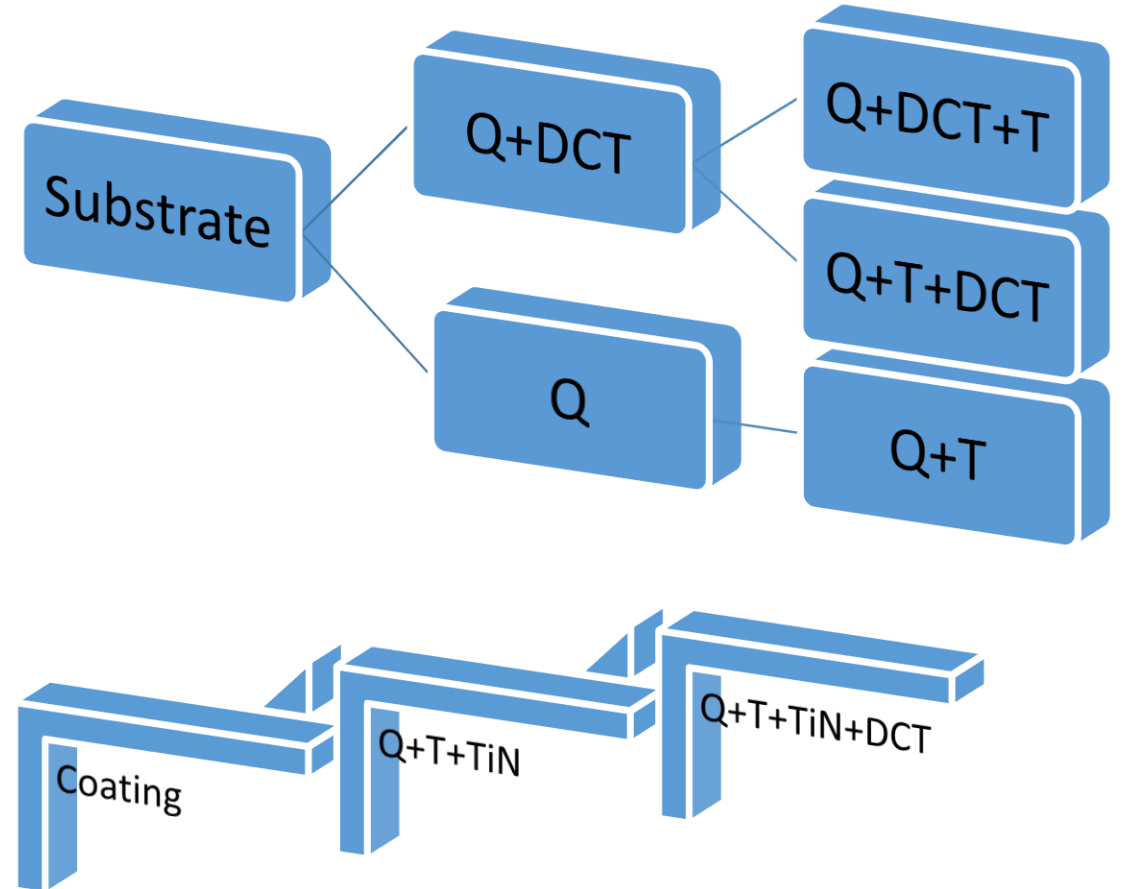
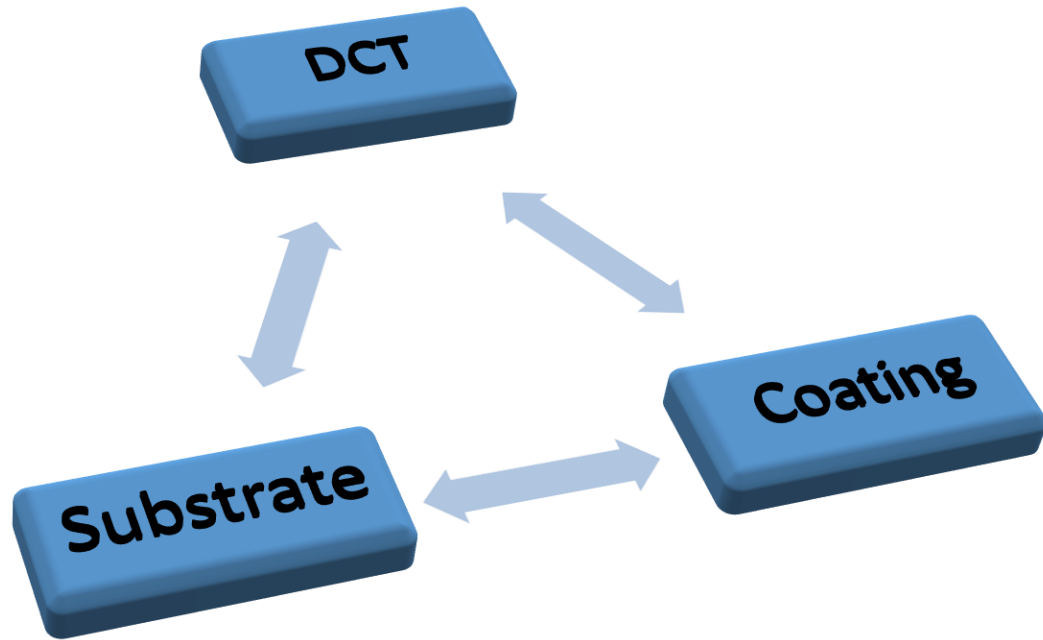
Treated tools	HRc	Untreated tools	HRc
A	66	D	66
B	65	E	65
C	66	F	66

(-196 °C/24 h) [6]

AISI M2 + TiN	DCT + TiN	153% tool life improvement
AISI M2 + TiN	TiN + DCT	109 % tool life improvement



# Approach



# Experimental workflow



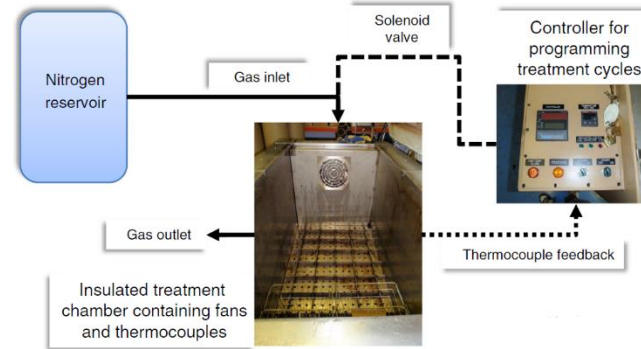
PVD

**Creation of material vapours**

**Transport of the vapours**

**Condensation of the vapours  
& Growth of coating**

Coating set up/ process [Ref 8]



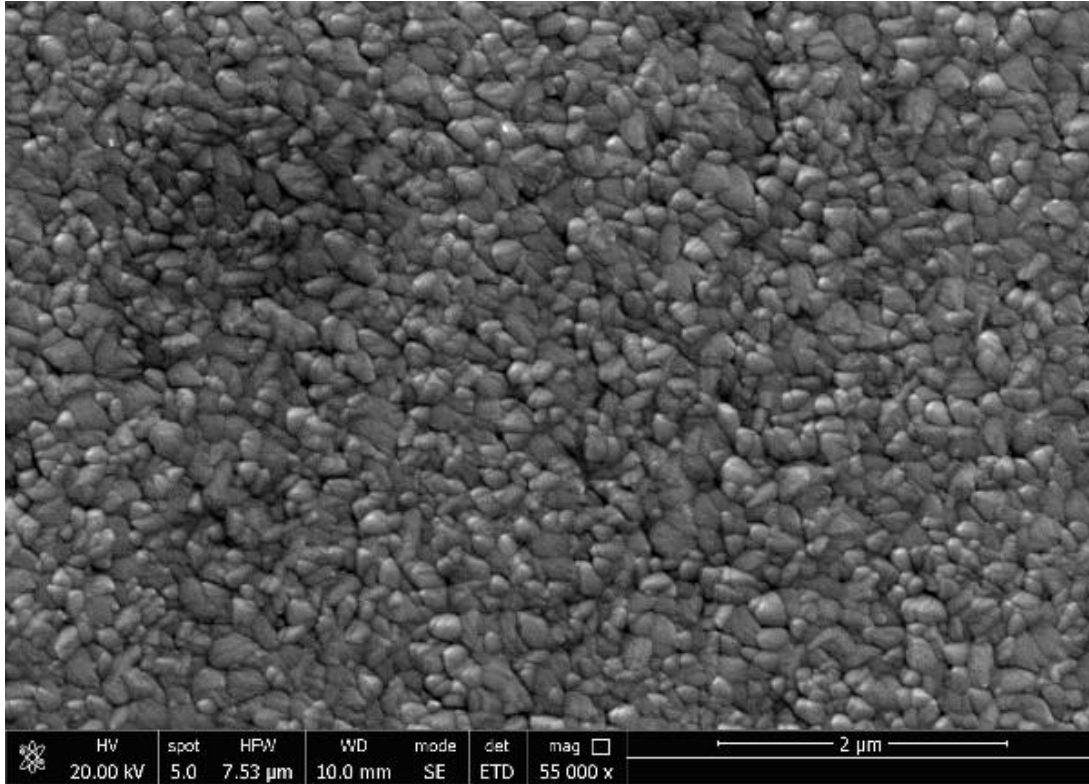
CT set up /technology [9]



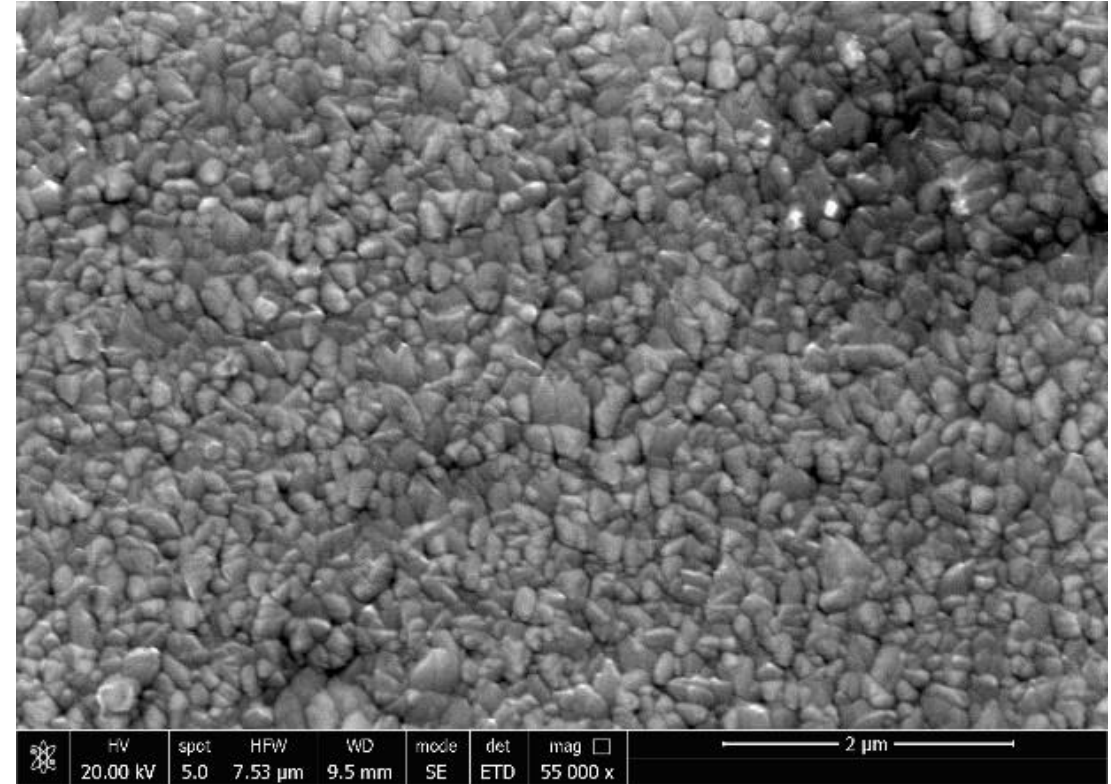
Result



# Results – Bulk structure

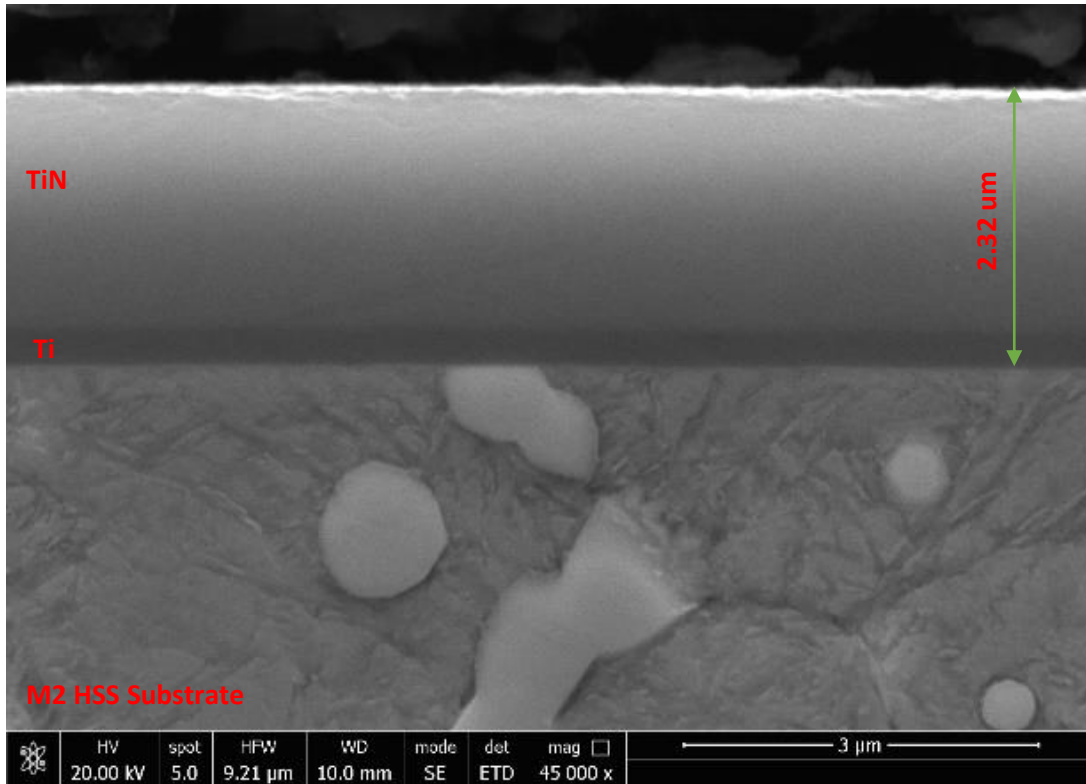


SEM Micrograph : Q+T+Coat – Coating surface

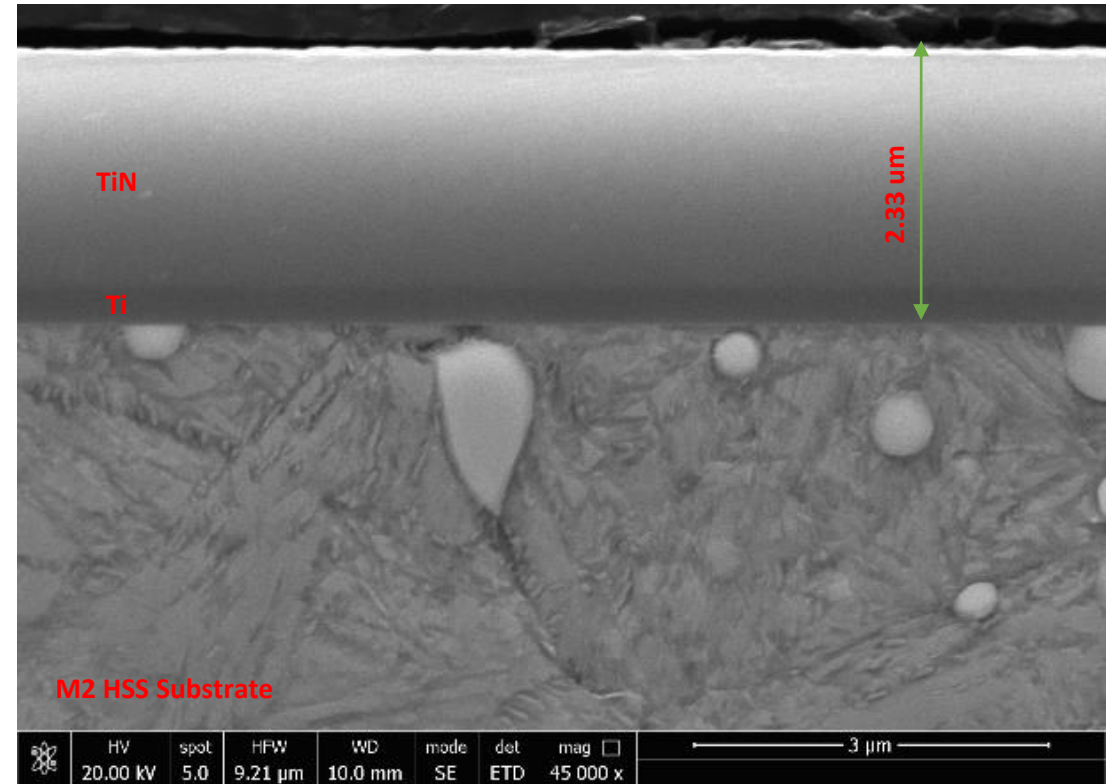


SEM Micrograph : Q+T+Coat+DCT – Coating surface

# Coating cross section



SEM micrograph: Q+T+Coat – Cross section



SEM micrograph: Q+T+Coat+DCT – Cross section

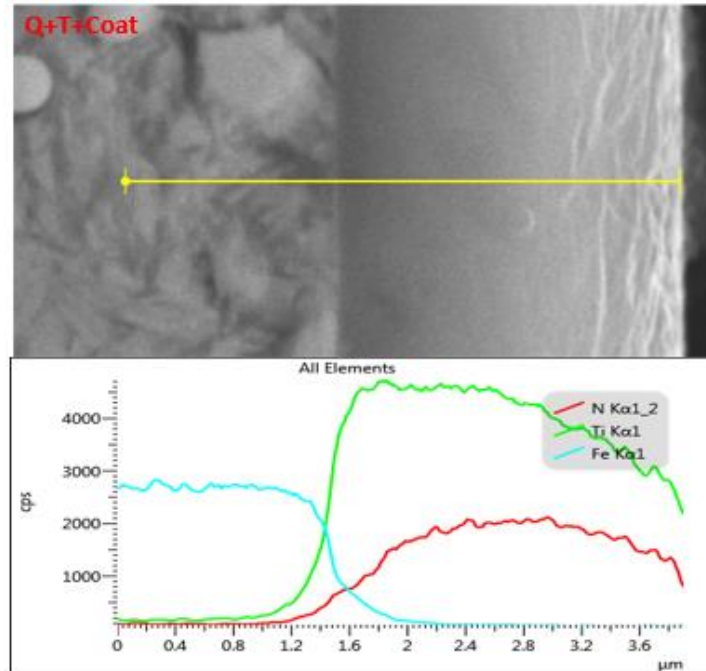
- Thickness - mean  $2.33 (\pm 0.01) \mu\text{m}$ , underlayer approx.  $298 (\pm 0.03) \text{nm}$

# Coating cross section

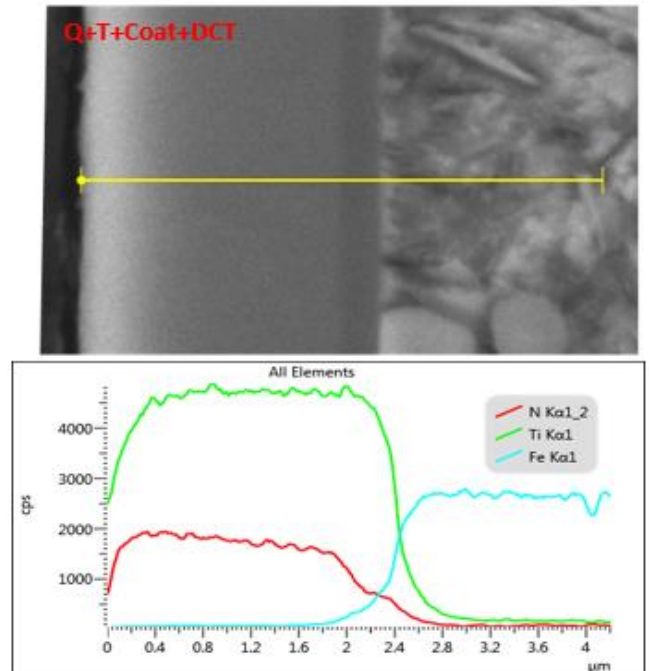


Surface roughness of the system and standard deviation

Material	Surface Roughness (Ra)
Q+T	$0.04 \pm 0.02$
Q+T+DCT	$0.04 \pm 0.02$
Q+T+Coat	$0.05 \pm 0.002$
Q+T+Coat+DCT	$0.05 \pm 0.001$



a) Line scan on cross section: Q+T+Coat



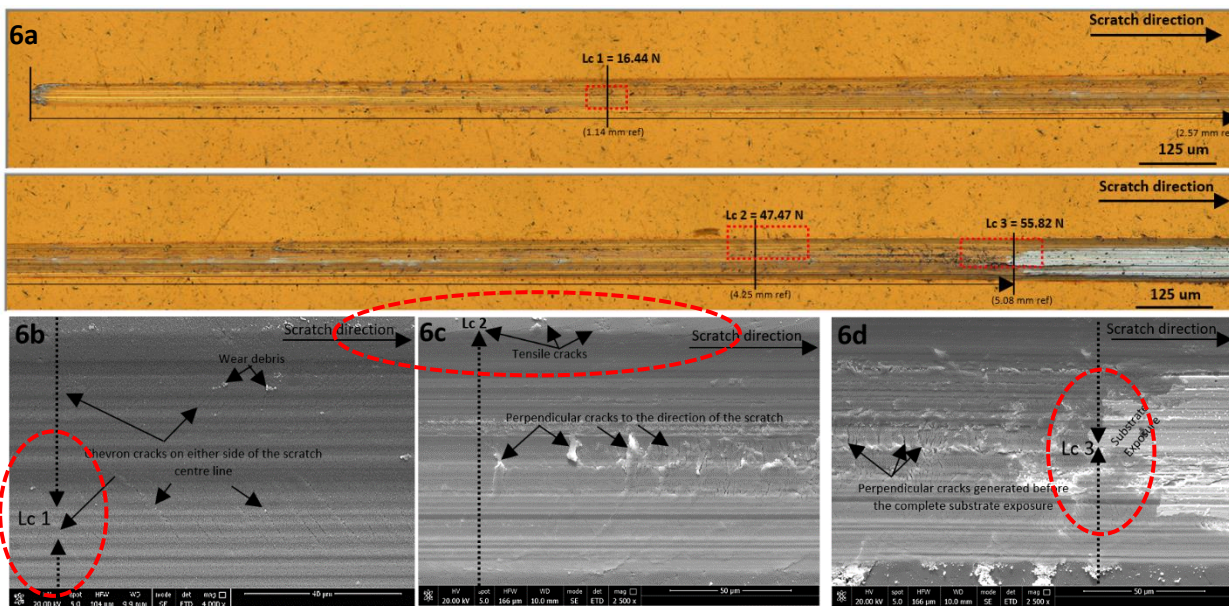
b) Line scan on cross section: Q+T+Coat+DCT



# Scratch tracks



Q+T+Coat



Q+T+Coat+DCT

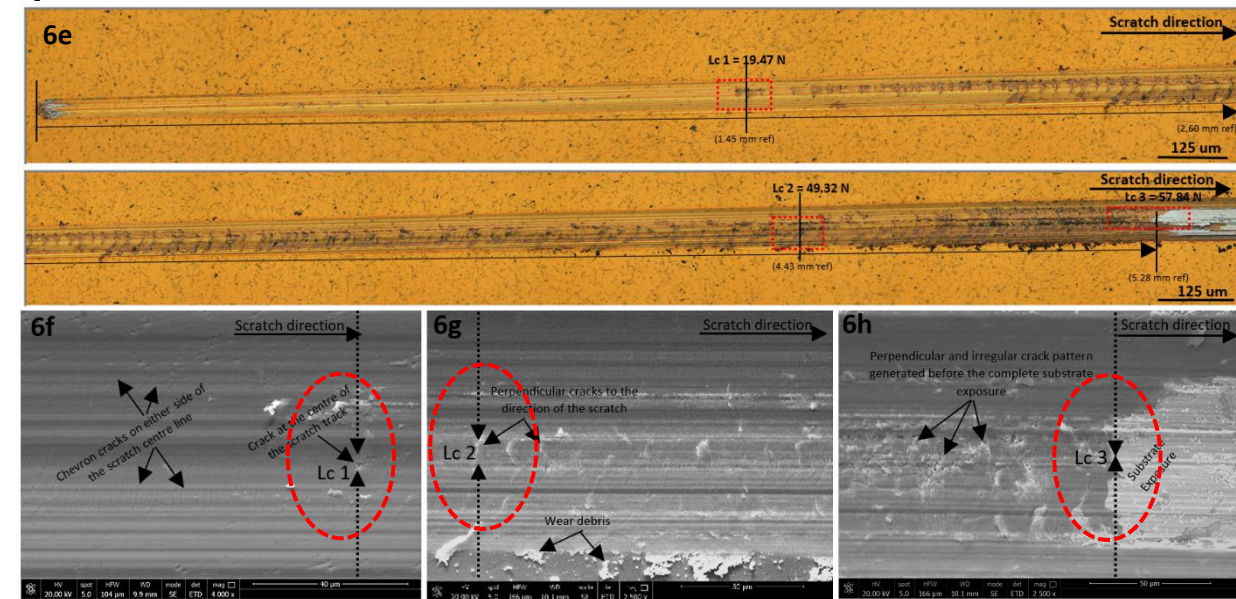


Fig. 6a Split up image from optical profiling microscope showing the scratch tracks to complete substrate exposure (for Q+T+Coat sample). SEM micrograph showing the Lc positions and cracks observed: (6b) Lc1 – 16.44 N (6c) Lc2 – 47.47 N (6d) Lc3 – 55.82 N (substrate exposure)

Fig. 6e Split up image from optical profiling microscope showing start of scratch tracks to the substrate exposure (for Q+T+Coat+DCT sample). SEM micrograph showing the Lc positions and cracks observed: (6f) Lc1 – 19.47 N (6g) Lc2 – 49.32 N (6h) Lc3 – 57.84 N (substrate exposure)



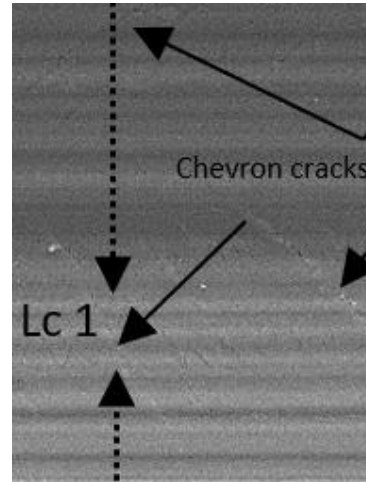
# Lc positions

Table: 1 Results of scratch test and standard deviation

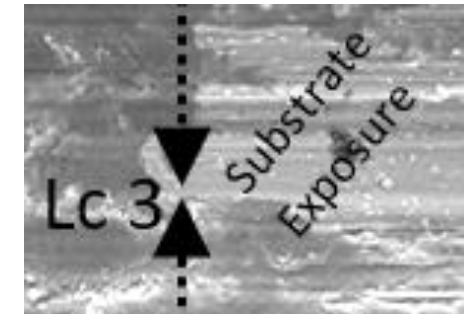
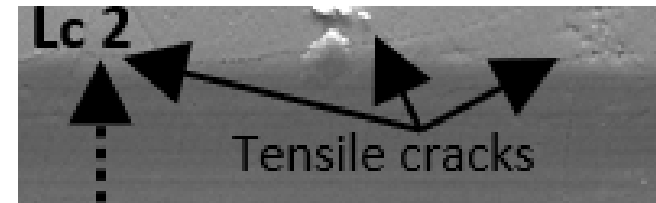
Samples	Lc1	Lc2	Lc3
Q+T+Coat	16.44 ± 2.08	47.47 ± 2.03	55.82 ± 2.92
Q+T+Coat+DCT	19.47 ± 1.70	49.32 ± 2.02	57.84 ± 3.11

Chevron, transverse and tensile cracks

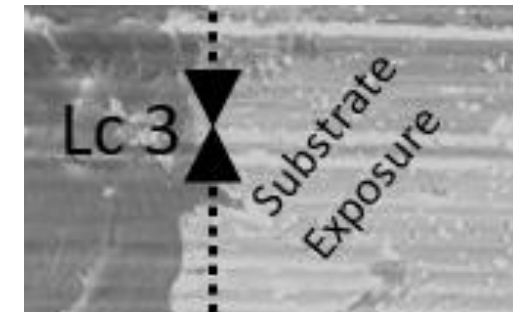
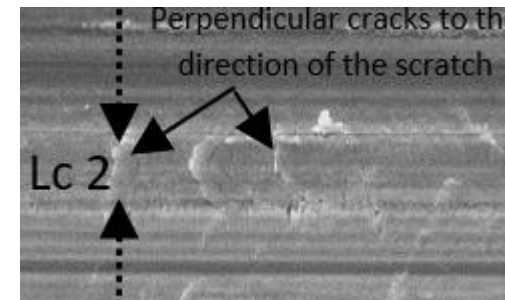
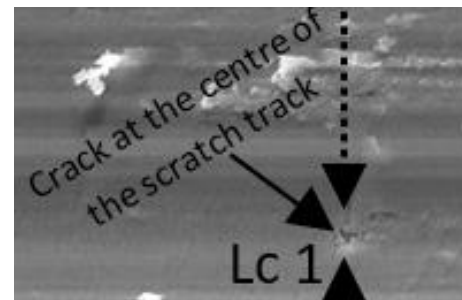
- Chevron cracks – either side of scratch centre line as well as cracks
- High Lc – irregular pattern cracks – fit into track and open away, perpendicular to the direction of the scratch.
- Denser and extensive
- Modulus and hardness



Q+T+Coat

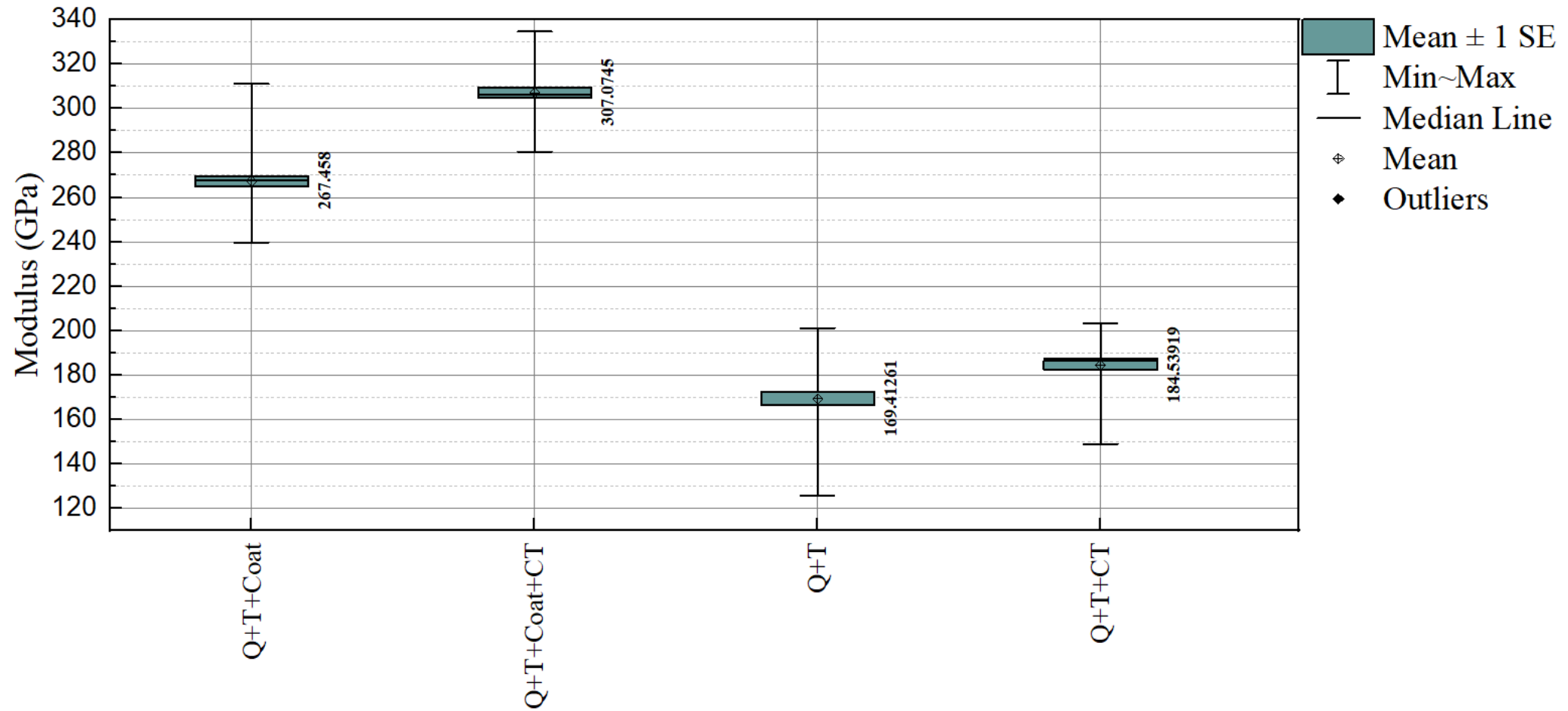


Q+T+Coat+DCT

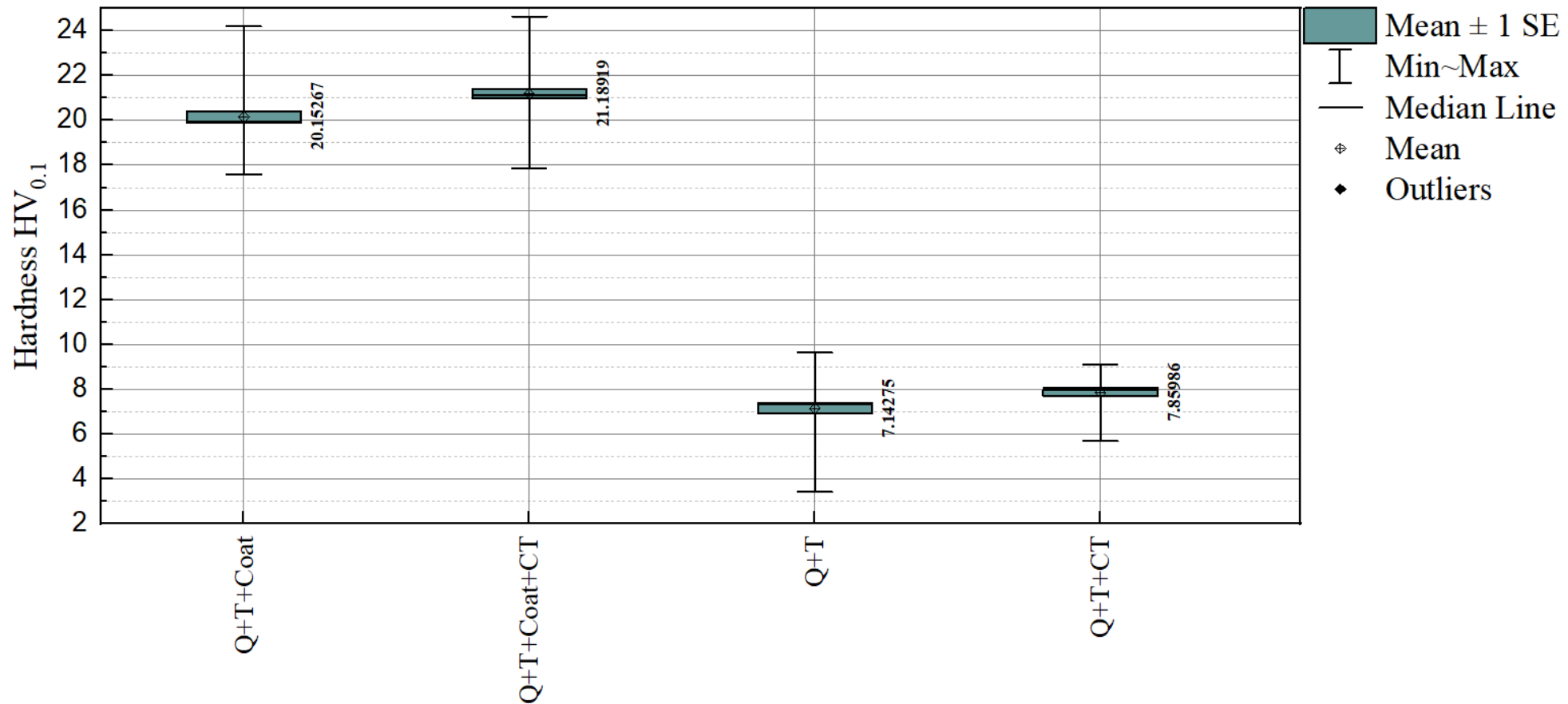




# Modulus Measurement



# Hardness Measurement



# Summary table of mechanical properties



Table: 2 Summary table of the measured mechanical properties of the system and standard deviation

Material condition (Coating/substrate)	Elastic modulus (GPa)	Indentation Hardness (GPa)	Elastic modulus ratio (GPa) – $E_{Co}/E_{Su}$
Q+T+Coat	267.46 ± 13.40	20.15 ± 1.46	--
Q+T+Coat+DCT	307.07 ± 14.05	21.19 ± 1.34	--
Q+T	169.41 ± 17.56	7.14 ± 1.21	--
Q+T+DCT	184.54 ± 13.06	7.86 ± 0.80	--
Q+T+Coat – $E_{Co}/E_{Su}$	--	--	1.58 ± 0.04
Q+T+Coat+DCT – $E_{Co}/E_{Su}$	--	--	1.66 ± 0.04

- Elastic modulus - Lc 1 and Lc 2
- Hardness - Lc 3
- 3.62%

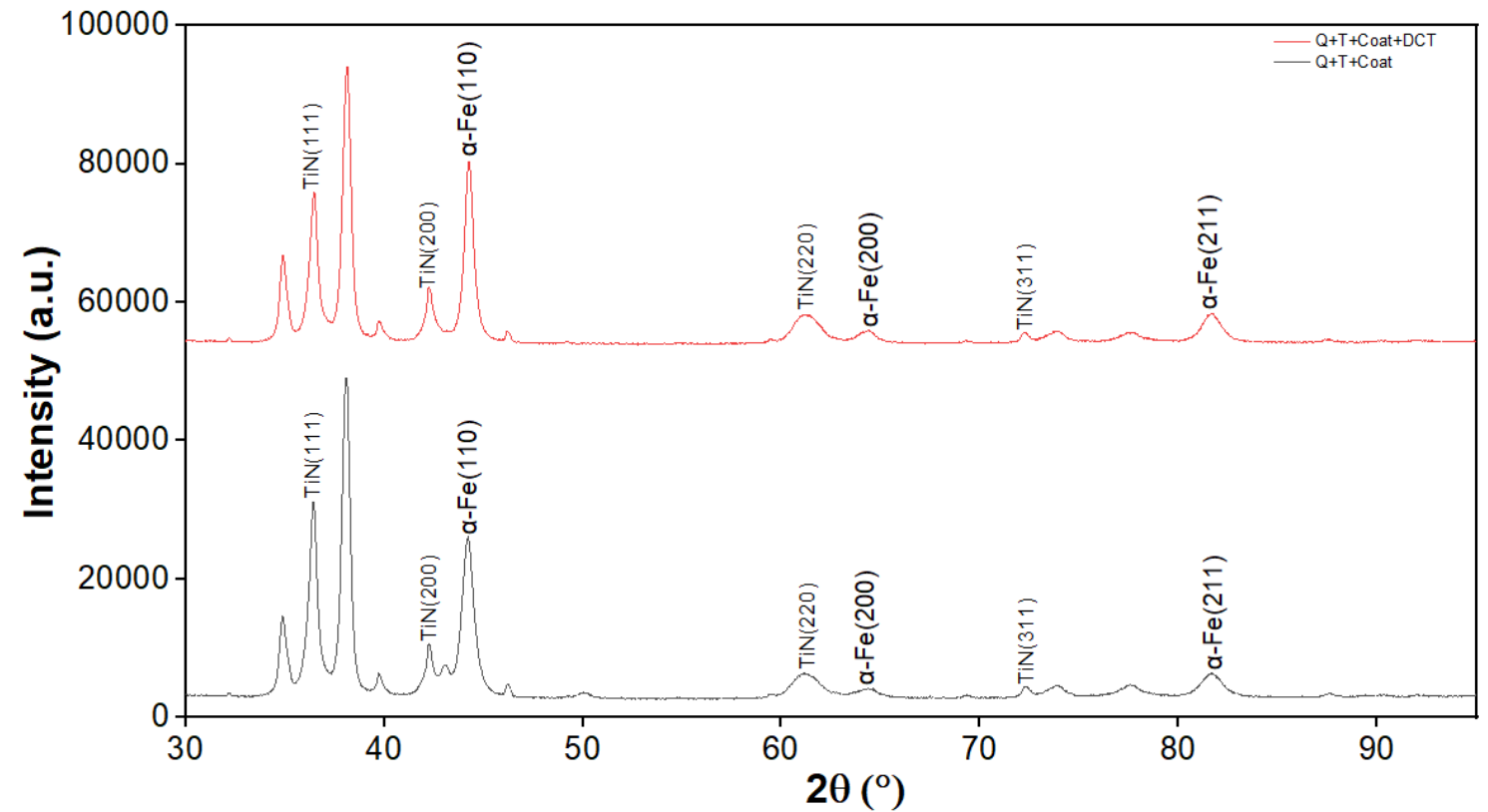
Table: 3 T-statistics for the measured values

T statistic	Test statistics (Q+T+Coat & Q+T+Coat+DCT) - Modulus	Test statistics (Q+T & Q+T+ DCT) - Modulus	Test statistics (Q+T+Coat & Q+T+ +Coat+DCT) - Hardness	Test statistics (Q+T & Q+T+ DCT) - Hardness
P - value	2.2572E-19	4.67168E-05	0.001248378	0.002026
Remark	Significant	Significant	Significant	Significant

# Diffraction pattern



- Q+T+Coat & Q+T+Coat+DCT exhibit similar pattern - Preferred orientation (111)
- TiN films: reflections corresponding to (111), (200), (220) and (311) was found at 36.51°, 42.57°, 61.37° and 72.26° respectively
- Substrate: reflections corresponding to (110), (200) and (211) assigned to 44.25°, 64.37° and 81.62° respectively



# W-H: Crystallite size and strain



$$\beta_T \cos \theta = \varepsilon(4 \sin \theta) + \frac{K\lambda}{L}$$

$$Y = mx + c$$

$$Y = \beta_T \cos \theta; m = \varepsilon; x = 4 \sin \theta; c = \frac{K\lambda}{L}$$

Where:  $\beta_T = \beta_D + \beta_\varepsilon$ ; and  $\beta_D = \frac{k\lambda}{L \cos \theta}$ ;  $\beta_\varepsilon = 4\varepsilon \tan \theta$ ;  $L = \frac{k\lambda}{\beta_D \cos \theta}$

$\beta_T$ : Total broadening of the peak (combine effect of broadening due to the crystallite size ( $\beta_D$ ) and broadening due to strain ( $\beta_\varepsilon$ ));

L: Average crystallite size;

K: shape factor (constant 0.9)

$\beta_D$ : full width at half maximum (FWHM) broadening of peak (radians);

$\theta$ : peak positions (radians).

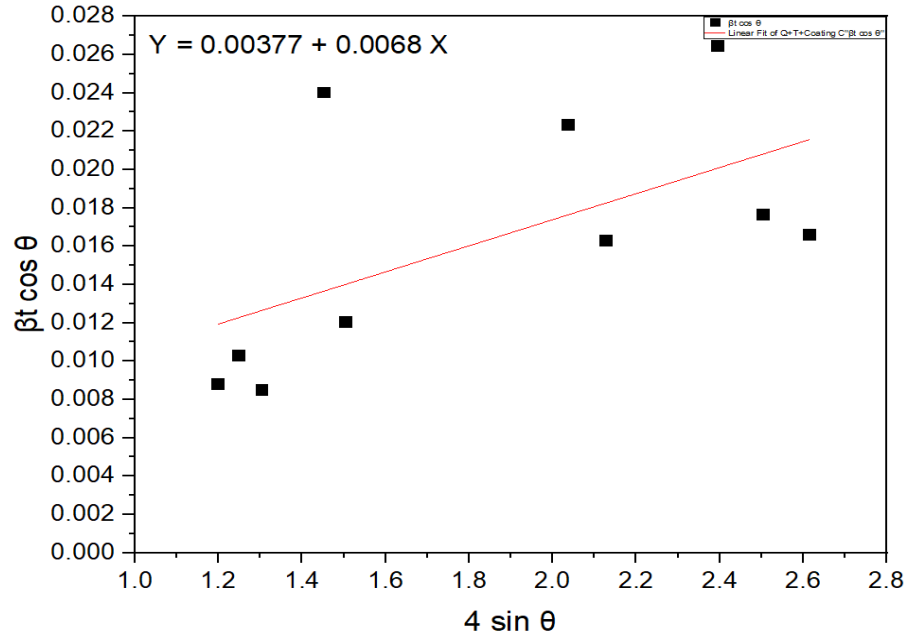
$\lambda$ : 0.15406 nm (x-ray source);  $\varepsilon$ : strain



# W-H: Crystallite size and strain



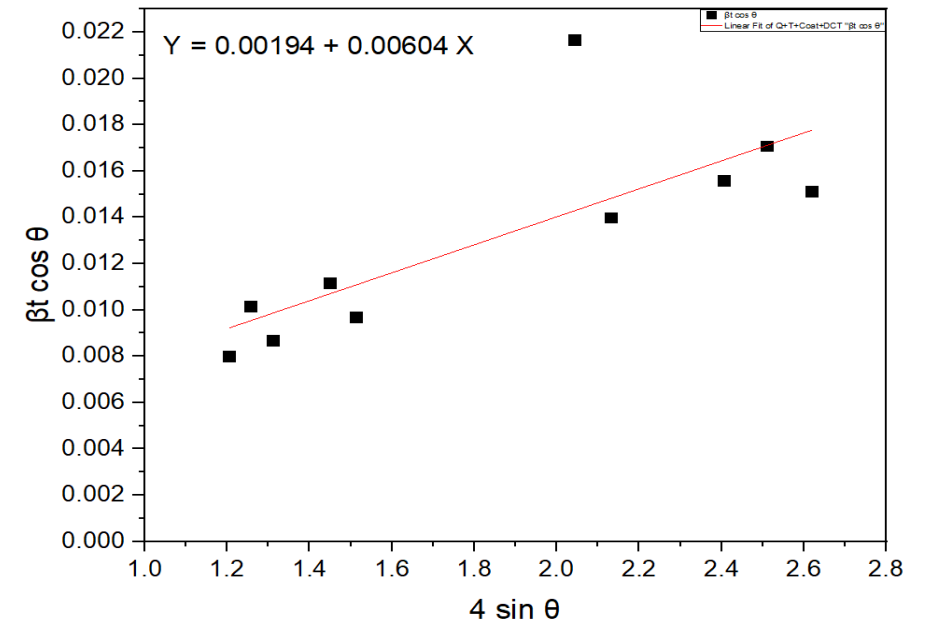
Q+T+Coat



Williamson hall equation

$$\beta_T \cos \theta = \varepsilon(4 \sin \theta) + \frac{K\lambda}{L}$$

Q+T+Coat+DCT



Plot of  $\beta_t \cos \theta$  against  $4 \sin \theta$  for Q+T+Coat

36.78 ( $\pm 8.76$ ) nm and strain of 0.00377 ( $\pm 0.00634$ ) %

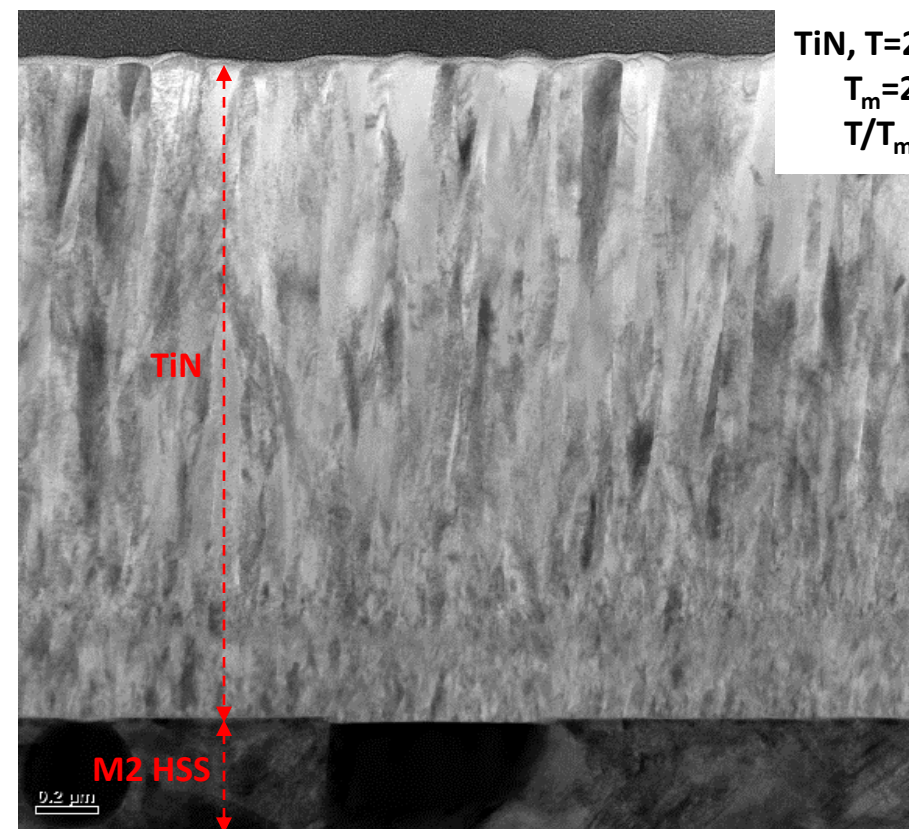
- Constant, more scatter away from the fit

Plot of  $\beta_t \cos \theta$  against  $4 \sin \theta$  for Q+T+Coat+DCT

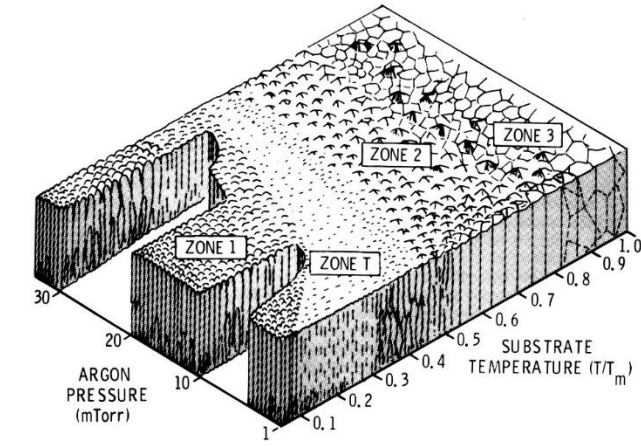
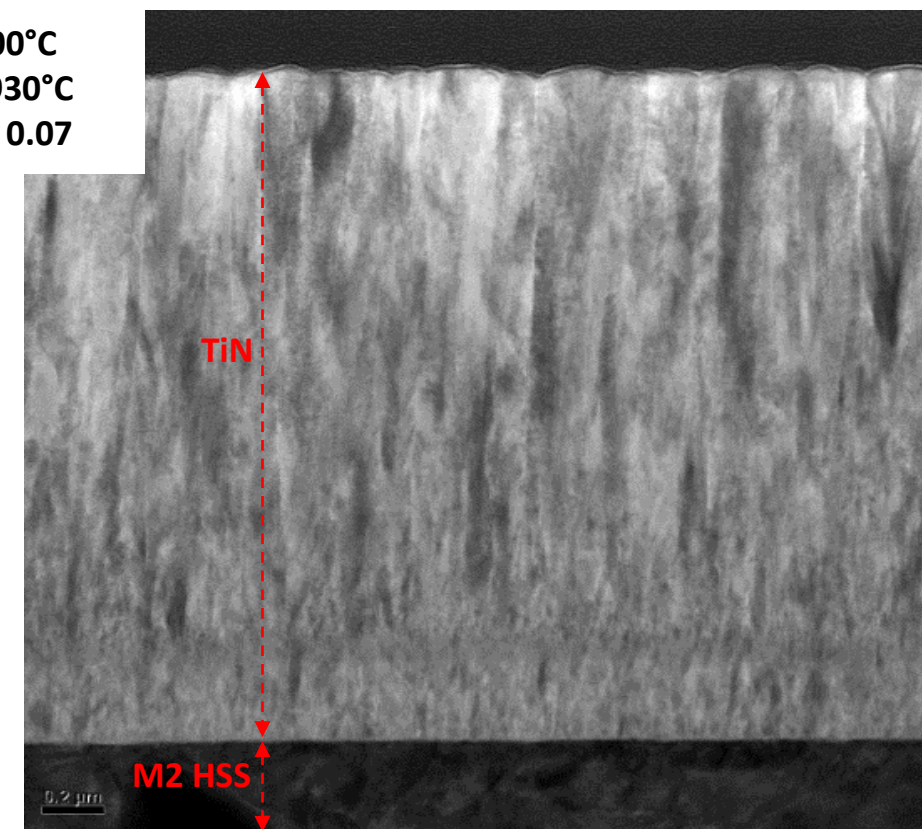
71.74 ( $\pm 1.76$ ) nm and strain of 0.00194 ( $\pm 0.00908$ ) %

- Constant, less scatter away from fit
- 71.47 ( $\pm 1.76$ ) nm, while strain decreased to 0.00194 ( $\pm 0.00908$ ) (0.49% reduction)

# Coating Morphology



TiN, T=200°C  
 $T_m=2930^\circ\text{C}$   
 $T/T_m=0.07$



Cross section of Q+T+Coat via TEM - 80 000 mag

Cross section of Q+T+Coat+DCT via TEM - 80 000 mag

## Structure zone Model 8]

- 1- Open fibrous like arrangement
- T-fine grained, densely packed fibrous grains
- 2-fairly dense columnar grains
- 3-large recrystallised equiaxed grains



- Improvement - 3.62%
- Combination of Elastic modulus and hardness
- Elastic modulus - Lc 1 and Lc 2
- Hardness - Lc 3





1. Collins, D. N. and Dormer, J., *Deep Cryogenic Treatment of a D2 Cold-work Tool Steel. Heat Treatment of Metals*. 1997. **3**: pp. 71-74.
2. Das, D., et al., *Effects of Deep Cryogenic Treatment on the Carbide Precipitation and Tribological Behaviour of D2 Steel*. *Materials and Manufacturing Processes*, 2007. **22**(4): pp. 474-480.
3. Gill, S.S., et al., *Effects of Deep Cryogenic Treatment on AISI M2 High Speed Steel: Metallurgical and Mechanical Characterization*. *Journal of Materials Engineering and Performance*, 2012. **21**(7): pp. 1320-1326.
4. Da Silva, F. J., et al., *Performance of Cryogenically treated HSS tools*. *Wear*, 2006. **261**(5): pp. 674-685.
5. Kelkar, R., et al., *Understanding the Effects of Cryogenic Treatment on M2 Tool Steel Properties*. *Heating Treating Progress*, 2007. **7**(5): pp. 57-60.
6. Mohan Lal, D., et al., *Cryogenic treatment on argument wear resistance of tool and die steels*. *Cryogenics*, 2001. **41**(1): pp. 149-155.
7. Zhang, Z. and Dong, H., *Surface Engineering Technologies*. IMPaCT CDT lecture slide - Bham, 2018.
8. Slatter, T., and Thornton, R., *Cryogenic Treatment of Engineering Materials in Comprehensive Materials Finishing*, M.S.J. Hashmi, Editor. 2017, Elsevier: Oxford. Pp. 421-454.

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- Advanced Microscopy Facility – University of Leicester
- Loughborough Materials Characterisation Centre – Loughborough University







*Thank you for your attention*

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